

FUNCTIONAL SERVICING AND STORMWATER MANAGEMENT REPORT

IN SUPPORT OF REZONING & SITE PLAN APPROVAL

Northumberland Mall

**Elgin St. West & Rogers Road
Cobourg, Ontario**



8395 Jane Street, Suite 100
Vaughan, Ontario L4K 5Y2
Tel: (905) 326-1404

File Number: 19046

Prepared For:

Trinity Development Group Inc.

No.	Revision	Date
2	Issued for Rezoning/Site Plan Approval	03/16/2020
1	Issued for Rezoning/Site Plan Approval	12/17/2019



Northumberland Mall
Cobourg, Ontario

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*Northumberland Mall
Cobourg, Ontario*

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- Overall Site Plan by Petroff Partnership Architects, Dated March 13, 2020
- Topographic Survey by SVNG Ltd., Dated October 25, 2019
- Buried Utility Map by Mark-It Located Inc., dated November 22, 2019

Appendix B – Stormwater Management Plans

- Pre-Development SWM Plan
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Appendix D – Water Demand Calculations

- Domestic Flow Calculations
- Fire Underwriters Survey Calculations



Introduction

1.1 Background

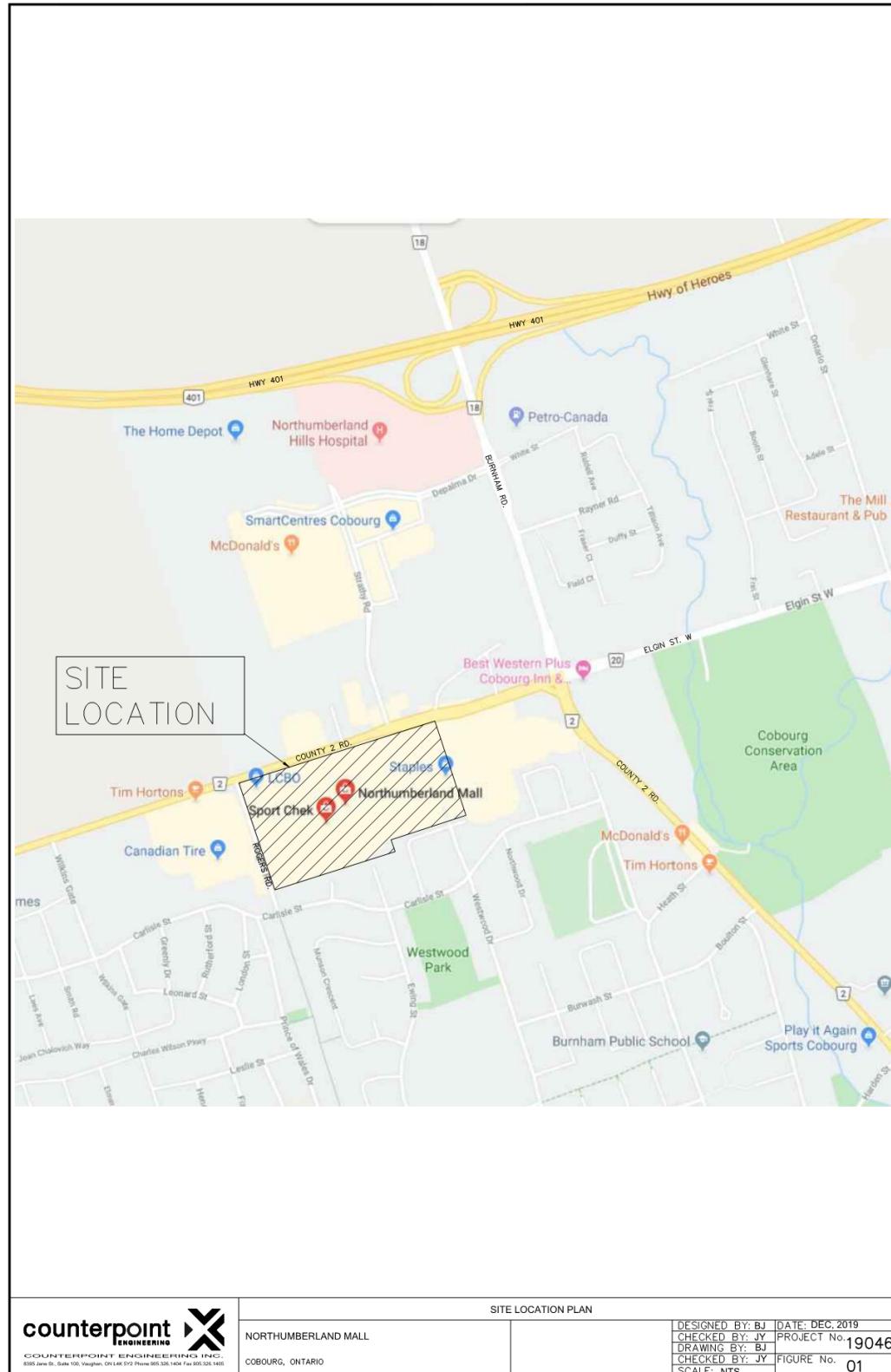
The Functional Servicing and Stormwater Management Report ('FSSWMR') has been prepared in support of rezoning and site plan approval for proposed retail unit and parking lot modifications as part of Northumberland Mall located on the south side of Elgin Street West, east of Rogers Road, in the Town of Cobourg. The limit of regrading is 0.81 Ha in size, consisting of 3 distinct areas:

- 1) Area 1: 0.39 Ha of area along the west side of the parking field including the existing entrance from Rogers Road;
- 2) Area 2: 0.39 Ha of Area east of the existing Boston Pizza and west of the signalized intersection/entrance from Elgin Street West. This includes a proposed multi-tenant unit, Building D;
- 3) 0.03 Ha of Area in the central area of the existing mall on the north side.

The proposed development will consist of relocating the Rogers Road entrance north and reconfiguring the parking layout (Area 1), and constructing a 929 m² building in Area 2. Area 3 consists of a slight expansion to the mall structure with required concrete apron and drive aisle regrading. Extension of water and sanitary services will be required from the existing infrastructure located within the property boundary east of the proposed building D. The proposed storm flows will be conveyed to the existing storm system in the subject site. Refer to **Figure 1 – Site Location Plan**.



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Cobourg, Ontario





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2 Stormwater Management

2.1 EXISTING CONDITIONS

The existing subject site consists mainly of asphalt area draining to site catchbasins and catchbasin manholes. Drainage characteristics in the pre-development condition for the areas of regrading is as follows:

2.1.1. Area 1

Stormwater in the existing condition is captured by catchbasins and catchbasin manholes connected to the 600 mm diameter storm sewer that runs north-south as per the Pre-Development SWM Plan (**Appendix B**). Drainage is conveyed south and east around the existing mall. Rogers Road is at a higher elevation relative to the mall, therefore no uncontrolled drainage contributes to the municipal Right-of-Way (ROW). The composite Runoff Coefficient is 0.85 for the 0.39 Ha of regraded area.

2.1.2. Area 2

Stormwater in the existing condition drains south to two (2) catchbasins on the north side of the main drive aisle encircling the mall (see Pre-Development SWM Plan in **Appendix B**). Drainage is conveyed downstream to the existing 450 mm diameter storm sewer and through the mall. Elgin Street is at a higher elevation relative to Area 2, therefore no uncontrolled drainage contributes to the municipal Right-of-Way (ROW). The composite Runoff Coefficient is 0.87 for the 0.39 Ha of regraded area.

See **Appendix B** for Pre-Development SWM Plan.

2.2 PROPOSED CONDITIONS

The proposed development will require regrading of the existing parking lot and entrances to accommodate the proposed layout as per the site plan by Petroff Partnership Architects (See



Appendix A). Drainage characteristics in the post-development condition for the areas of regrading is as follows:

2.2.1. Area 1

The proposed development for Area 1 consists of moving the existing entrance at Rogers Road to the north. New catchbasins (CB5 and CB6) are added due to the need to regrade the parking field, and are connected to the same 600 mm storm sewer as in the pre-development condition. As well, an existing catchbasin will be replaced with a double catchbasin (DCB7) and connected to the 600 mm storm sewer as a result of its increased tributary area.

For Area 1, all drainage in the existing and proposed condition is captured and conveyed to the same downstream 600 mm storm sewer. The runoff coefficient in the post-development condition decreased to 0.78 (0.85 in the pre-development condition) and therefore the contributing flow rate decreased as well. See **Appendix B for Detailed Pre and Post-Development Drainage Plans.**

2.2.2. Area 2

The proposed development for Area 2 consists of a new building D with a drive-thru, and various parking, concrete walkway, and landscaped areas. As is typical for this type of development, roof drainage from Building D will be controlled at 42 L/s/ha and conveyed to the existing storm manhole east of the entrance drive aisle from Elgin Street West. Additionally, drainage from catchbasins 1 to 3 and catchbasin manhole 4 will also be conveyed to the existing storm manhole, as there are no storm sewers in the vicinity of the proposed area of regrading. A portion of the concrete apron and parking area will continue to flow overland south to the same existing catchbasins as in the pre-development conditions. For Area 2, all drainage in the existing and proposed condition is captured and conveyed to the 450 mm storm sewer in the main drive aisle before flowing downstream through the mall. See Locates Plan by Mark-It Locates Inc. in **Appendix A and Post-Development Drainage Plan in Appendix B** for existing



servicing and proposed stormwater management plans. The runoff coefficient in the post-development condition is decreased to 0.76 (0.87 in the pre-development condition) and therefore the flow rate decreased as well.

The minor system capacity was analyzed for impacts resulting from regrading in Area 1 and 2 and concluded that the proposed condition provides an adequate level of service. In conclusion, downstream sewers will have improved capacity as a result of the increased landscaped area onsite and controlled rooftop drainage from building D. Grading in Area 3 does not require analysis as the 0.03 ha area is 100% impervious in both the pre- and post-development conditions. As well, any area where asphalt is removed and replaced without regrading was not analyzed as the drainage conditions do not change in the post-development condition (i.e. heavy-duty asphalt added in new fire routes).

Additionally, proposed stormwater sewer sizing has been reviewed as per OBC criteria and calculations are included in **Appendix B**. As per these calculations, the proposed storm sewers are adequately sized for the proposed development.

3 SANITARY SERVICING

3.1 EXISTING CONDITIONS

A 300 mm diameter sanitary sewer exists east of the Elgin Street South entrance, adjacent to the A&W. This sewer flows east and south around the existing mall.

3.2 PROPOSED CONDITIONS

A 150 mm diameter sanitary sewer will be connected to the existing sanitary manhole and extended across the north-south drive aisle as per the Site Servicing Plan. The MOE and Town of Cobourg do not have standards for calculating equivalent population of small commercial developments, so the City of Toronto's Design Criteria for Sewers and Watermains were used. Based on guidelines of 1.1 persons/100 m² of floor space, the proposed Building D has an



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equivalent population of 10.2. Using an average domestic sewage flow of 450 litres/capita/day (the max as per MOE Sewage Works, page 5-10), the proposed building generates **4,590 litres/day** of sanitary flow or **0.053 l/s**. When including an infiltration allowance of 0.26 l/s/Ha (typical) and a peaking factor of 3.8 (maximum as per Town of Cobourg Design Guidelines, p.26), the site has a peak sanitary flow of **0.2985 l/s (See Appendix C)**.

The sanitary sewer immediately downstream of the connection to the existing manhole is a 150 mm diameter pipe with a slope of 0.77%. Typically, a pipe of this size has capacity for **13.364 L/s**. At peak hours, the building D peak sanitary flow (with infiltration) of 0.2985 l/s is **2.2%** of the full-flow capacity.

4 WATERMAIN SERVICING

4.1 EXISTING CONDITIONS

A 150 mm diameter watermain exists east of the Elgin Street South entrance, adjacent to the A&W.

4.2 PROPOSED CONDITIONS

A new 150 mm diameter PVC watermain is to be connected to the 150 mm diameter watermain via tee. The expected domestic water usage rate for the post-development condition of the site was calculated using the maximum **450 L/c/day** demand. Using a population of **10.2** the commercial demand is **4,590 l/day**. Applying a maximum day factor of 9.5 (maximum per MOE Design Guidelines for Drinking Water Systems, p. 3-9), the Total Maximum Daily water demand is 43,605 l/day or **30 l/min**. Applying a maximum hour factor of 14.13 (maximum as per MOE), the Peak Hour water demand is 64,857 L/day or **45 L/min**. Refer to Appendix C.1 for domestic usage calculations.



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Fire flow demand was estimated using the Fire Underwriters Survey ('FUS') guidelines. Using an area of **929 m²** the fire flow was calculated as **6,705 l/min** before reductions. No reductions or charges results in a total Fire Flow demand of **7,000 l/min** (rounded to nearest 1,000 L/min).

As per the Town of Cobourg Design Guidelines page 48, watermains shall be sized to carry the greater of maximum day or maximum hour plus fire flow. Therefore, the total demand for the proposed development is **7,045 l/min** or **1,861 USGPM**. Refer to **Appendix D** for supporting FUS calculations. The FUS parameters for reductions utilized in this report must be re-visited during detailed building design to confirm any changes that may be required to the FUS calculations.

It is recommended that a hydrant flow test be completed during detailed building design to confirm that the existing system provides sufficient fire protection.



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5 CONCLUSION

As indicated in the provided functional servicing and stormwater management report, the proposed storm, sanitary and water concept is capable to support the re-zoning and site plan of the subject site for the parking lot modifications and proposed building D.

We trust this report sufficiently addresses all aspects of the site servicing in support of re-zoning site plan approval.

Sincerely,



Jude Yoganathan, P.Eng

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Email: jyoganathan@counterpointeng.com



Ben Jackson, P.Eng

Direct: 416-702-1260

Email: bjackson@counterpointeng.com



Functional Servicing Report
Northumberland Mall, Cobourg, Ontario

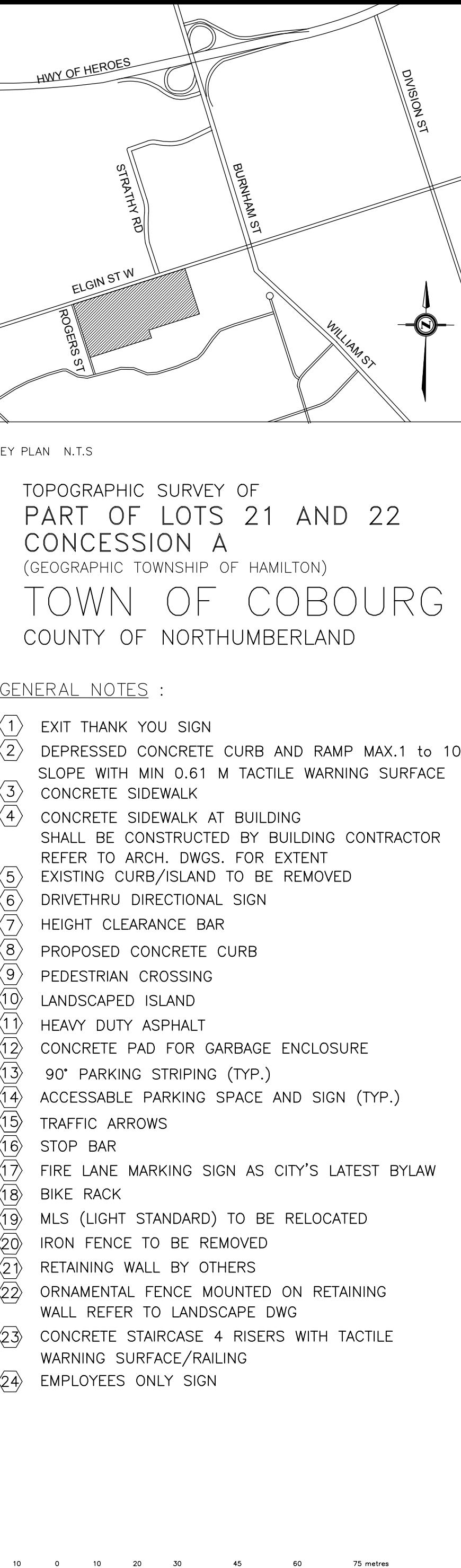
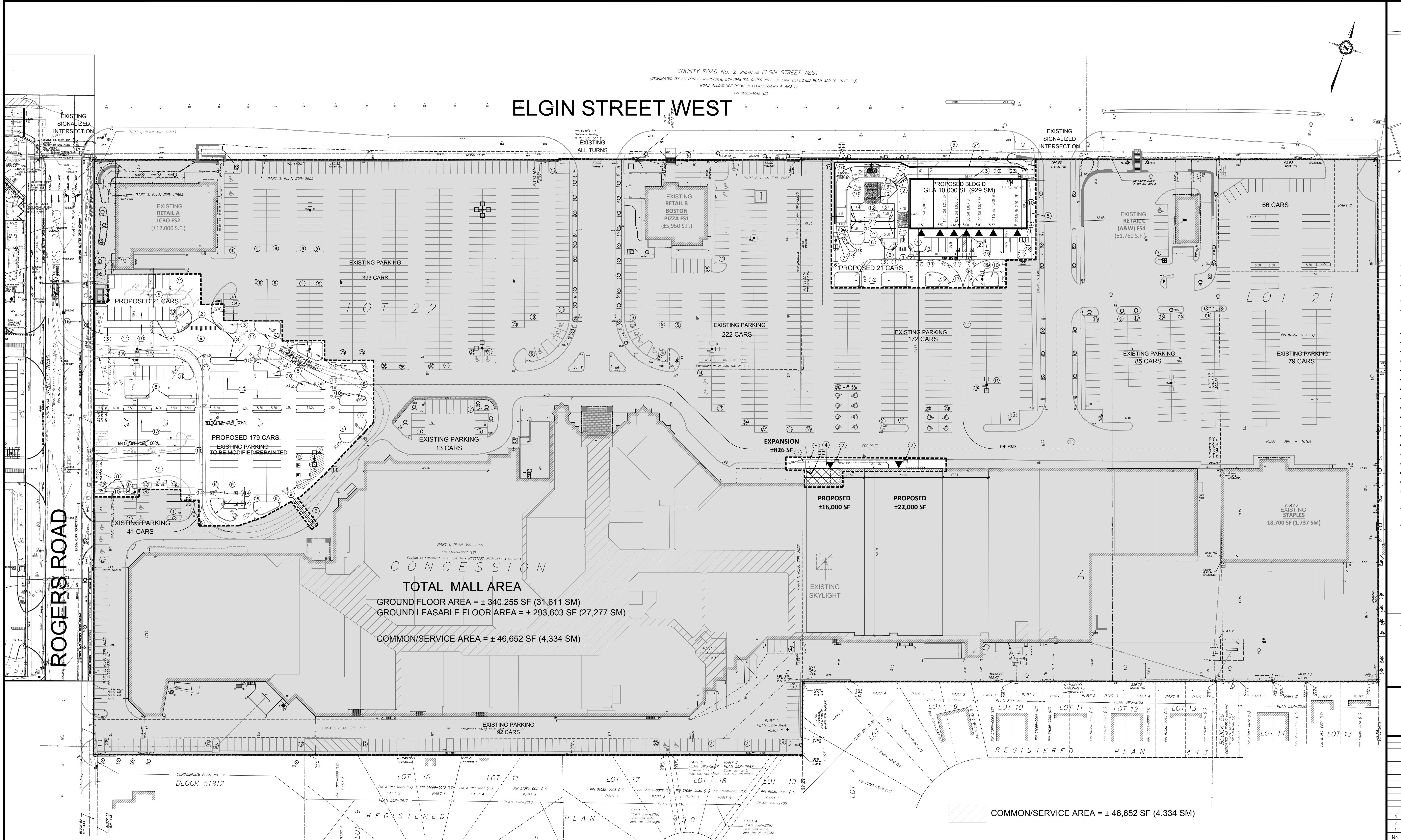
APPENDICES



Functional Servicing Report
Northumberland Mall, Cobourg, Ontario

Appendix A

Site Plan and Surveys



TRINITY

3. REVISED AS PER COTC COMMENTS MAR. 13, 2020 DR
 2. ISSUED FOR SITE PLAN APPROVAL DEC. 16, 2019 DR
 1. ISSUED FOR ZONING REVIEW JULY 30, 2019 DR

No. REVISIONS MARK VOID ALL COPIES PREVIOUS FINAL DATE DATE BY

Contractor must check and verify all dimensions on the job and report any discrepancies before proceeding with the work.

Do not scale the drawing.

This drawing contains copyright material belonging to the Architect.

This drawing shall not be reproduced in whole or in part without the written approval of the Architect.

This drawing was developed for a specific purpose; use for any other purpose is not permitted.

This drawing must be read in the context of all the other drawings which constitute the document.

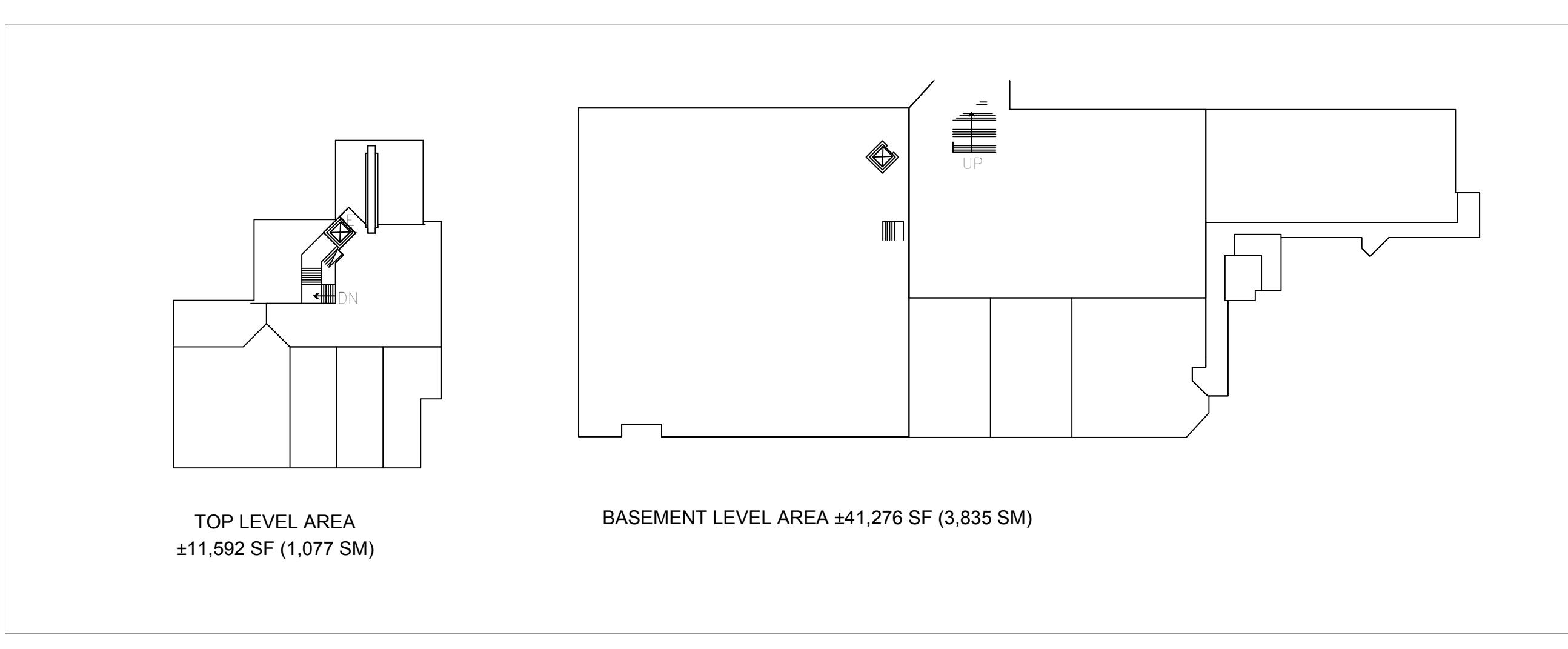
ALY HAMDY LICENCE #768

260 TOWN CENTRE BLVD. SUITE 300
 MARKHAM ONTARIO CANADA L3R 8H8
 TEL. 905.470.7000 FAX. 905.470.2500

DRAWN BY	DR
CHECKED BY	AH
DATE	MAY 16, 2019
ISSUED	MARCH 13, 2020

19060
SA-010

OVERALL SITE PLAN
SCALE: 1:600



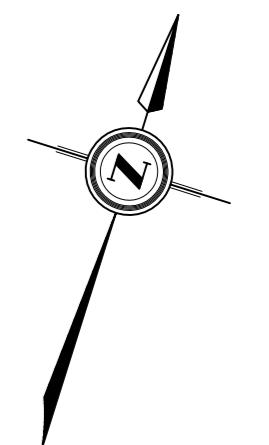
TOPOGRAPHIC SURVEY OF
PART OF LOTS 21 AND 22
CONCESSION A
(GEOGRAPHIC TOWNSHIP OF HAMILTON)

TOWN OF COBOURG
COUNTY OF NORTHUMBERLAND

SCALE 1 : 500
0 10 20 30 40 50 metres


SPEIGHT, VAN NOSTRAND & GIBSON LIMITED
ONTARIO LAND SURVEYORS
2019

(C) THE RETROACTIVE ALTERATION OR USE OF THIS PLAT IS PROHIBITED
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SPEIGHT, VAN NOSTRAND & GIBSON LIMITED. IT IS STRICTLY PROHIBITED




COUNTY ROAD No. 2 KNOWN AS ELGIN STREET WEST
(DESIGNATED BY AN ORDER-IN-COUNCIL OC-1949/RD/01 DATED NOV. 30, 1949 DEPOSITED PLAN 320 (P-1947-1))
(ROAD ALLOWANCE BETWEEN CONCESSIONS A AND 1)

PIN 51089-1045 (LT)



Metric
DISTANCES SHOWN ON THIS PLAN
ARE IN METRES. THEY ARE NOT CONVERTED
TO FEET BY DIVIDING BY 0.3048



MARK IT
LOCATED INC.

Utility Mapping Quality Levels
as per ASCE C-1 38-02

QL-A Locating exact vertical and horizontal position of underground utilities using appropriate safe excavation techniques and recording these data.

QL-B Designating approximate position of underground utilities by the application of appropriate surface geophysical methods.

- Limited in scope to verification of provided level D information.
- Utilities may escape detection. (See Notes)

QL-C Survey of surface features.

QL-D Records and plans research including record collection and review.

Notes:

- This information is provided for design purposes only.
- This information is not a substitute for sanctioned locates as required by law.
- Prior to any excavation, all utility owners must be contacted to verify the location of their respective utilities and obtain Health & Safety Act compliant safe work practices.
- The estimated locations indicated on this drawing are only estimates and should be verified by direct physical exposure.
- The spatial accuracy of the plotted information is dependent on the surveying methods used to collect the data.
- The spatial accuracy of the plotted information is dependent on the best effort, best-practices basis, within the constraints of the surveying methods used to collect the data.
- This information is provided on a best effort basis within the constraints of the surveying methods used to collect the data.
- This information is provided on a best effort basis within the constraints of the surveying methods used to collect the data.
- The spatial accuracy of the plotted information is dependent on the best effort, best-practices basis, within the constraints of the surveying methods used to collect the data.
- Known utilities existing at this site as of the drawing date.
- Locates Inc. is not responsible for any damage to known utilities existing at this site as of the drawing date.
- Locates Inc. during the course of this investigation.

SYMBOLS LEGEND	UTILITY CODES LEGEND
MANHOLE	W WATER
CATCH BASIN	E ELECTRIC
POLE	T TELEPHONE
CLEAN OUT	C COMMUNICATION CABLES/DUCT
STREET LIGHT	ALL ALL STREAM
HYDRANT	F/O FIBER OPTIC
VALVE	GS GAS SERVICE
TRANSFORMER	GM GAS MAN
HAND WELL	DZL DIESEL
PEDESTAL	TNP TRANS NORTHERN PIPELINE
CONTROL BOX / PLUG	FL FUEL LINE
VALVE CHAMBER	SAN SANITARY SEWER
TRAFFIC BOX	ST STORM SEWER
AIR PUMP	VI KEEPING TIE
SIGN	COMB COMBINATION SEWER
BUS SHELTER	IR IRRIGATION
TRAFFIC CONTROL BOX	U UNKNOWN SERVICE
FLUSH TO GRADE VAULT	TC TRAFFIC CONTROL
HEADWALL	
FLOW	
UTILITY CONTINUES	
TEST PIT	

Buried Utility Map

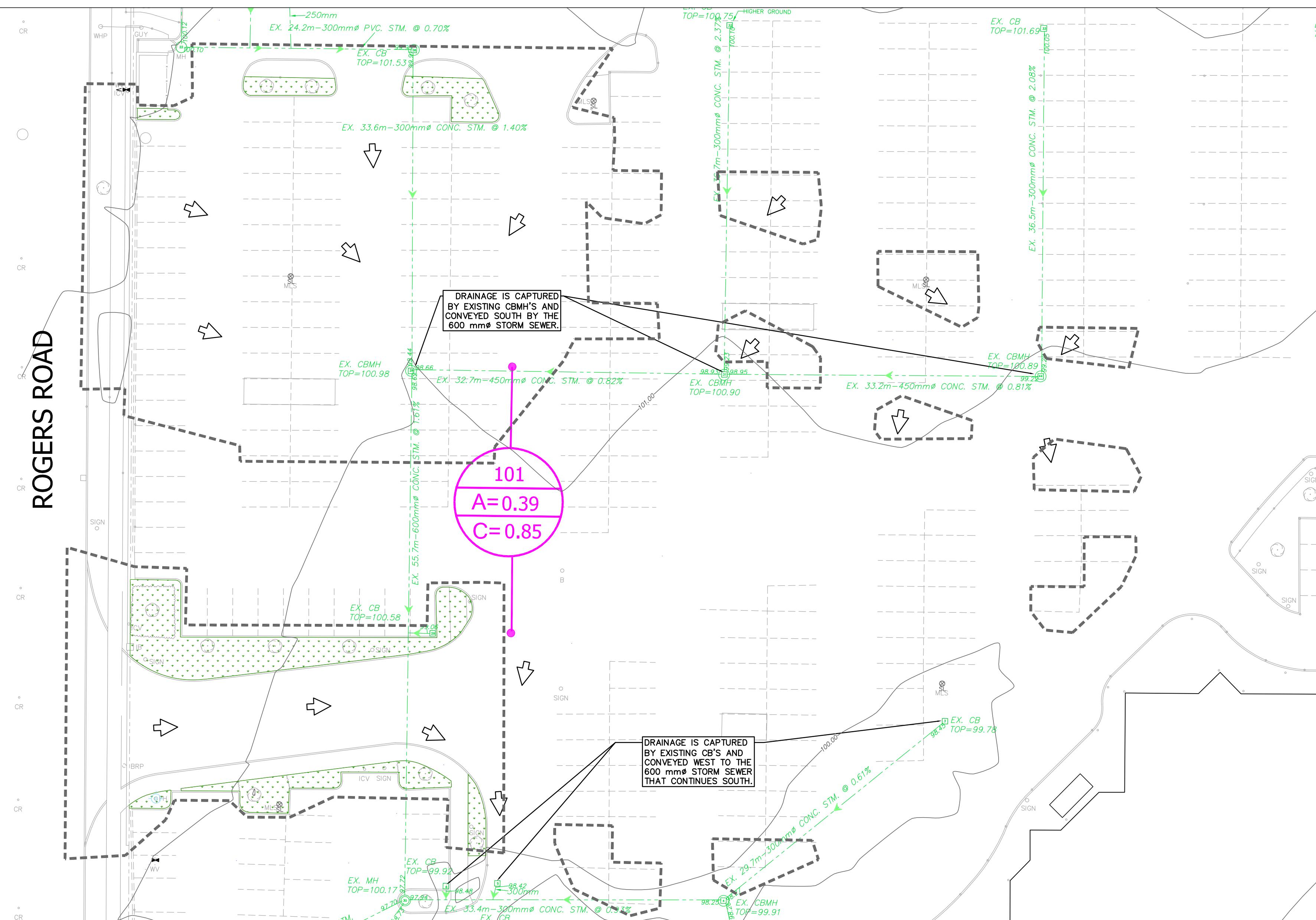
For: Trinity Development Group Site: 1111 Elgin Street West, Cobourg, ON
Project#2019-0926 Date: NOV 22, 2019 Checked: AC / SI



Functional Servicing Report
Northumberland Mall, Cobourg, Ontario

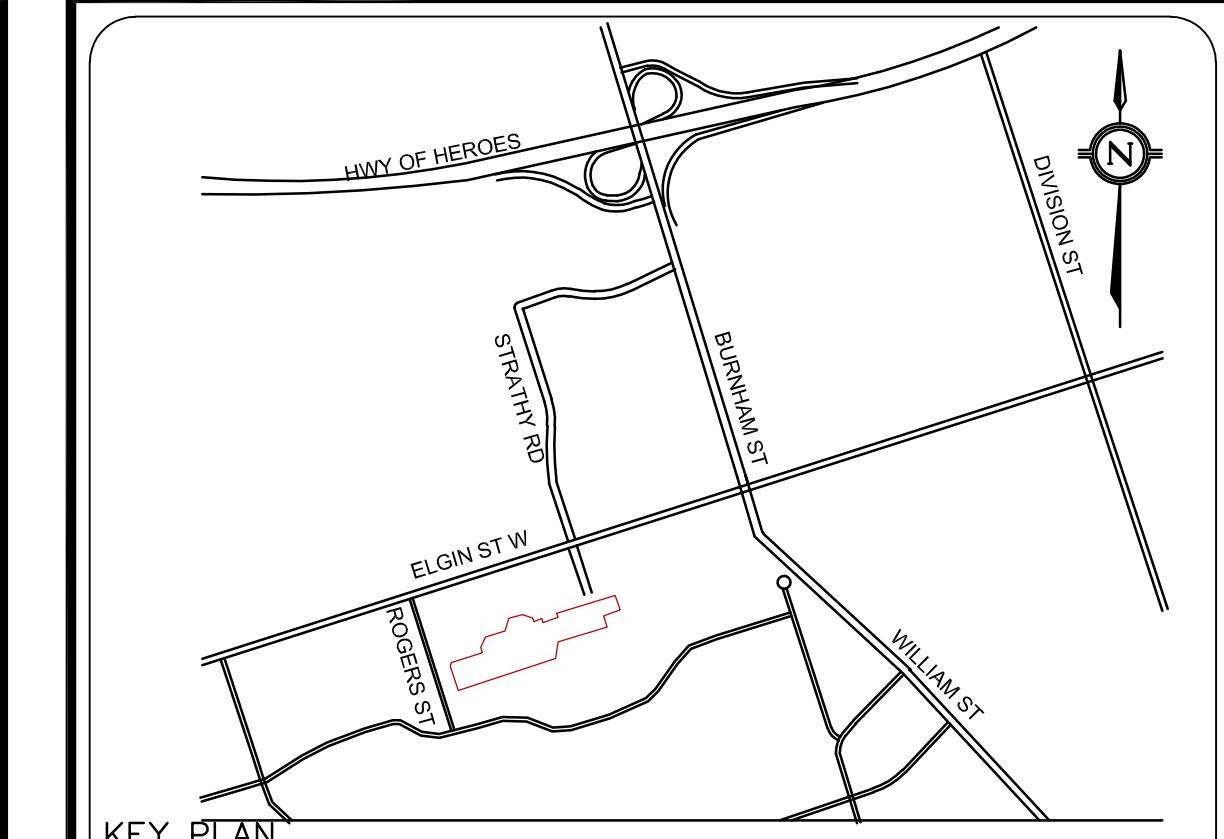
Appendix B

Stormwater Management Figures

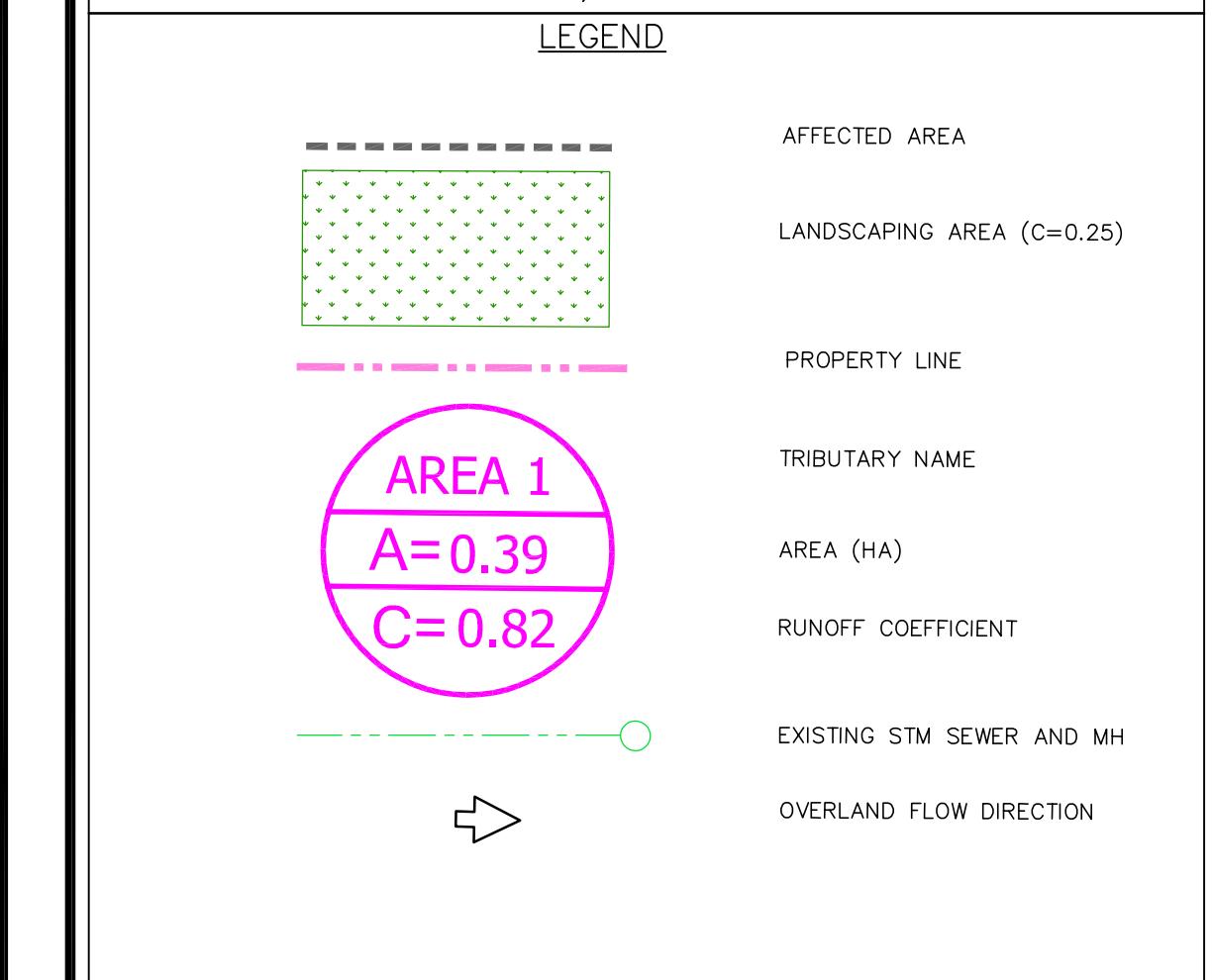


AREA 1: WEST ENTRANCE

LAND USE	AREA (Ha)	RUNOFF COEFFICIENT
LANDSCAPING AREA	0.03	0.25
CONCRETE/ASPHALT AREA	0.36	0.90
COMPOSITE (AFFECTED AREA)	0.39	0.85



SITE PLAN: SA-01.0: MARCH 13, 2020



2. ISSUED FOR SPA/ZBA #2 03/18/20 BJ
1. ISSUED FOR SPA/ZBA 12/17/19 BJ
No. DATE BY CITY

counterpoint ENGINEERING
COUNTERPOINT ENGINEERING INC.
8395 Jane St., Suite 100, Vaughan, ON L4K 5Y2 Phone 905.326.1404 Fax 905.326.1405



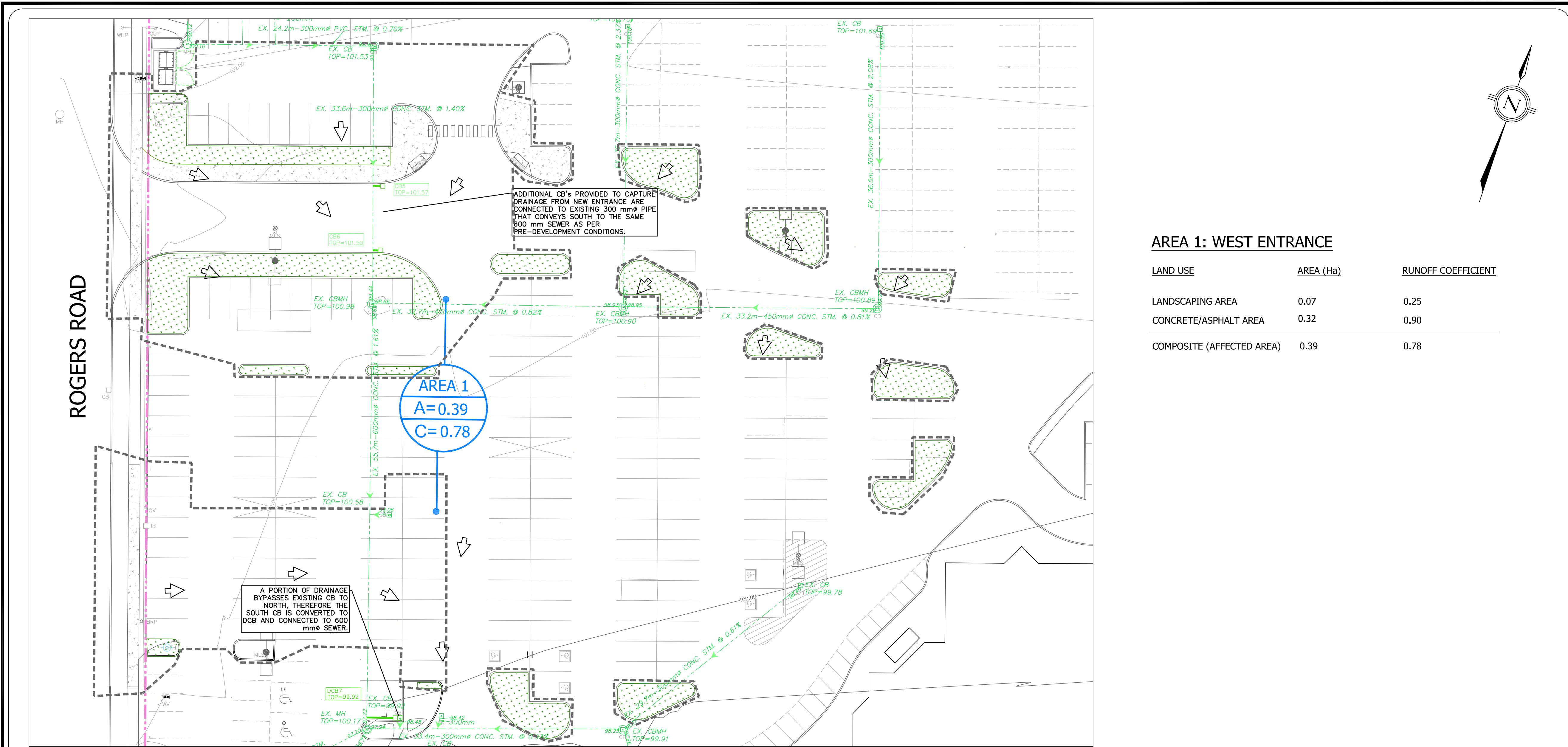
APPLICANT:
TRINITY DEVELOPMENT GROUP INC.
77 BLOOR STREET WEST
SUITE 1601
TORONTO, ON
M5S 1M2

SITE LOCATION:
NORTHUMBERLAND MALL
ELGIN ST. WEST AND ROGERS ROAD
COBOURG, ON.

SITE PLAN FILE No.: SPA-01-20

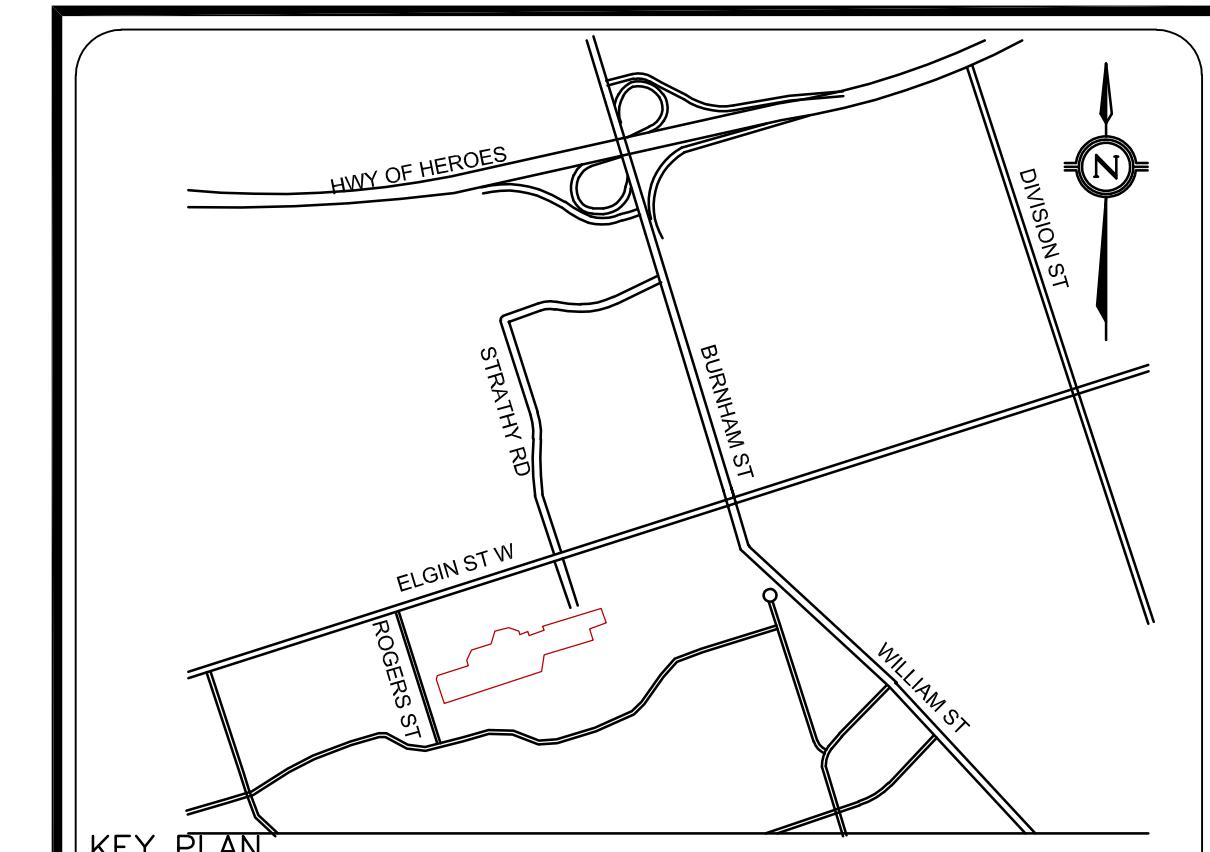
PRE DEVELOPMENT SWM PLAN

DESIGNED BY: AL	CHECKED BY: JY	DATE: MAR, 2020
DRAWING BY: AL	CHECKED BY: JY	PROJECT NO. 19046
SWM BY: BJ	CHECKED BY: JY	
SCALE: 1:300m	0m 5m 10m 15m	DRAWING NO. SWM-PRE



AREA 1: WEST ENTRANCE

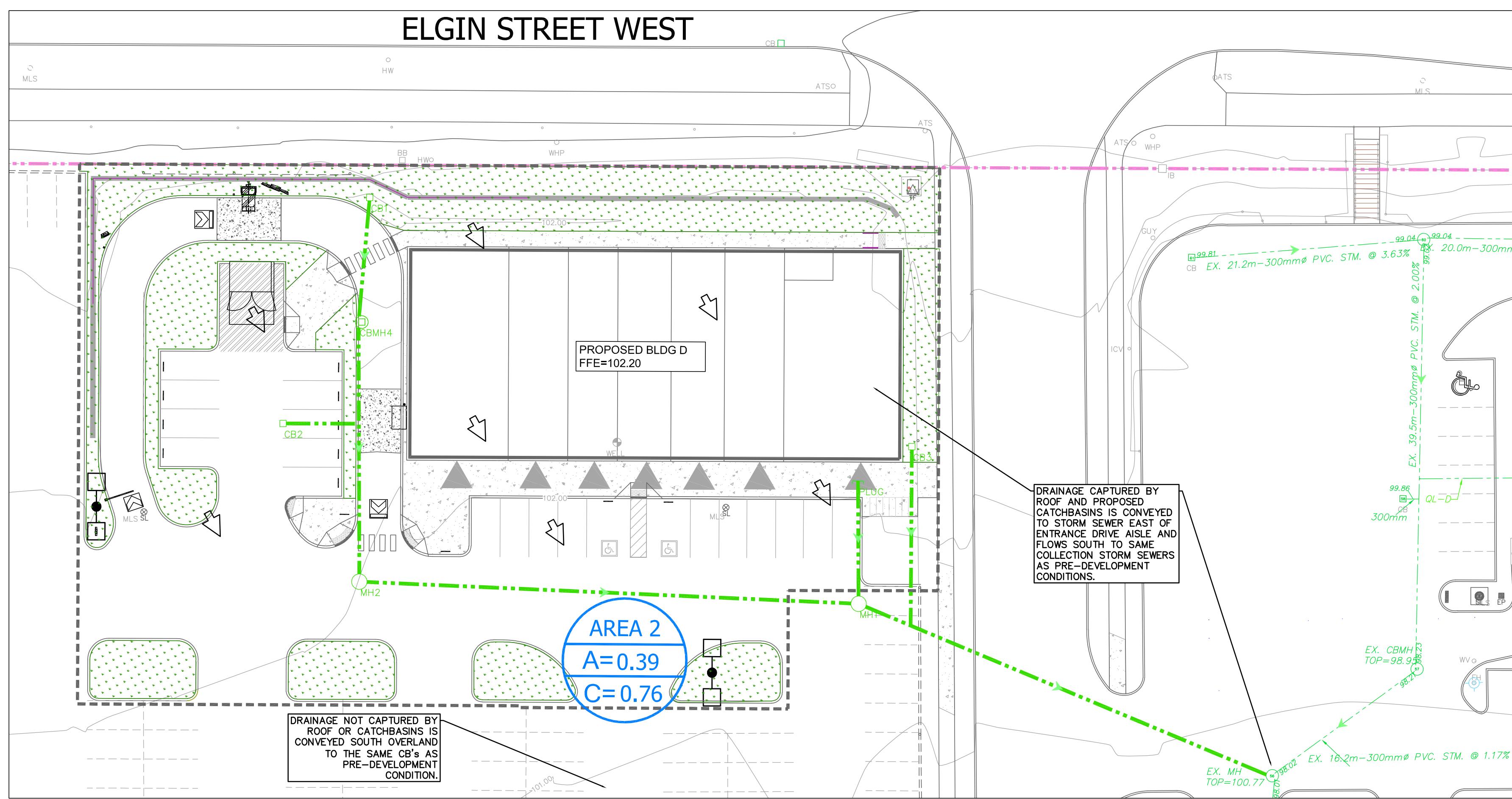
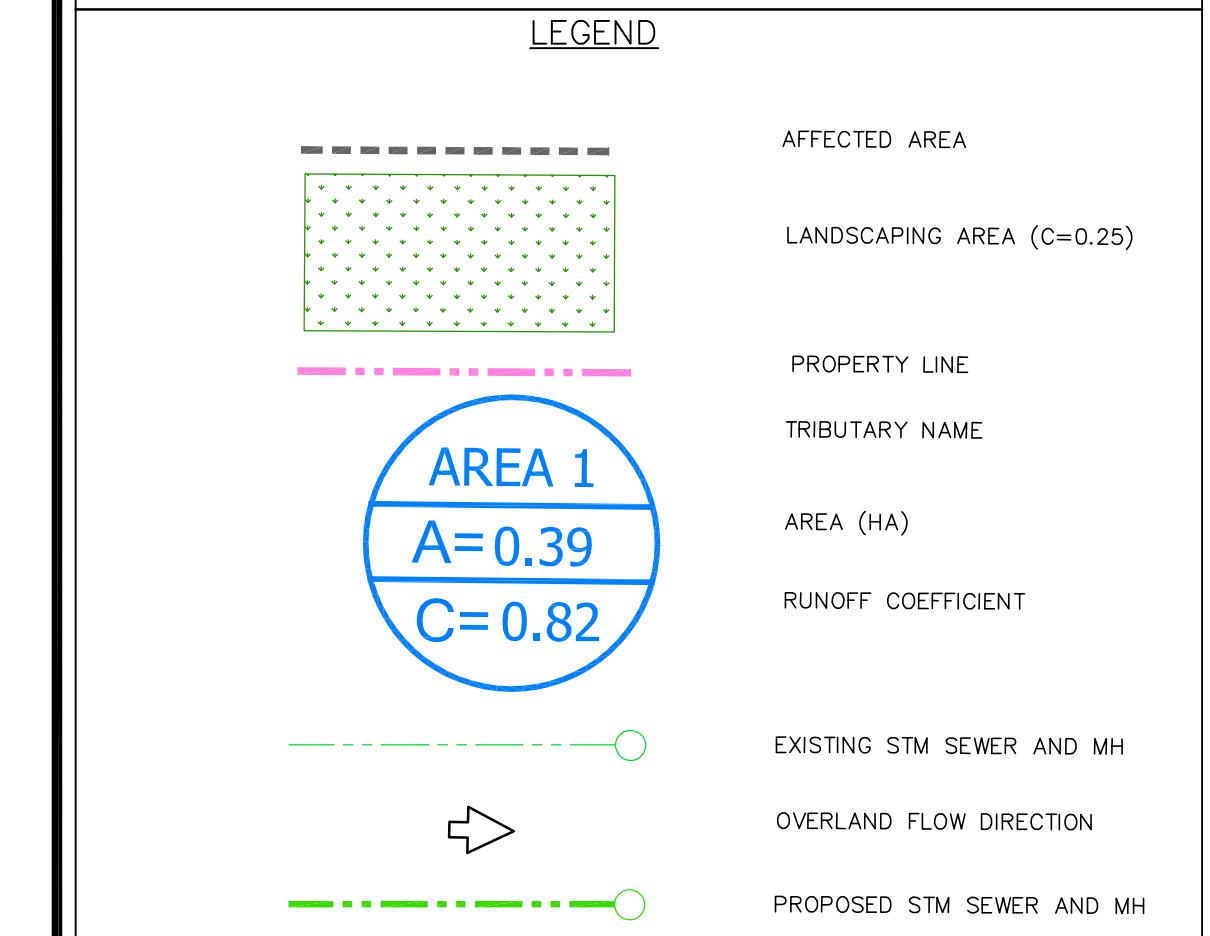
LAND USE	AREA (Ha)	RUNOFF COEFFICIENT
LANDSCAPING AREA	0.07	0.25
CONCRETE/ASPHALT AREA	0.32	0.90
COMPOSITE (AFFECTED AREA)	0.39	0.78



KEY PLAN
LEGAL & TOPOGRAPHY
PROVIDED BY: SVNG LTD.
750 OAKDALE ROAD
UNIT 66
TORONTO, ONTARIO
BENCHMARK
NOTE: ELEVATIONS ARE BASED ON GEODETIC DATUM FROM TOWN BENCH MARK 713012B AT AN ELEVATION OF 109.563.

BEARING NOTE
BEARINGS ARE ASTROMIC AND ARE REFERRED TO THE SOUTHERLY LIMIT OF ELGIN STREET AS SHOWN ON PLAN 39R-2955, HAVING A BEARING OF N71°46'50"E.

SITE PLAN: SA-01.0: MARCH 13, 2020



AREA 2: PROPOSED CRU

LAND USE	AREA (Ha)	RUNOFF COEFFICIENT
LANDSCAPING AREA	0.09	0.25
CONCRETE/ASPHALT AREA	0.30	0.90
COMPOSITE (AFFECTED AREA)	0.39	0.76

2. ISSUED FOR SPA/ZBA #2 03/18/20 BJ
1. ISSUED FOR SPA/ZBA 12/17/19 BJ
No. REVISIONS/ISSUED DATE BY CITY

counterpoint ENGINEERING
COUNTERPOINT ENGINEERING INC.
8395 Jane St., Suite 100, Vaughan, ON L4K 5Y2 Phone 905.326.1404 Fax 905.326.1405

LICENSED PROFESSIONAL ENGINEER
J. S. YOGANATHAN
100100545
MAI 16/20
PROVINCE OF ONTARIO
ENGINEER'S STAMP

APPLICANT:
TRINITY DEVELOPMENT GROUP INC.
77 BLOOR STREET WEST
SUITE 1601
TORONTO, ON
M5S 1M2

SITE LOCATION:
NORTHUMBERLAND MALL
ELGIN ST. WEST AND ROGERS ROAD
COBOURG, ON.

SITE PLAN FILE No.: SPA-01-20

POST-DEVELOPMENT SWM PLAN

DESIGNED BY: AL	CHECKED BY: JY	DATE: MAR, 2020
DRAWING BY: AL	CHECKED BY: JY	PROJECT NO. 19046
SWM BY: BJ	CHECKED BY: JY	
SCALE: 1:300m	0m 5m 10m 15m	DRAWING NO. SWM-POST

OBC Calculations

The following calculations review the capacity of the proposed 300 mm storm sewer between MH1 and the ex. MH southwest of the existing A&W. The upstream stormwater contributions to this pipe consist of tributary areas to CB1, CB2, CB3, CBMH4 and roof area of proposed building D (including vertical projection of the building walls).

7.4.10.4

- 1) Except as provided in sentence (2), the hydraulic load from a roof or paved surface is the maximum 15 min rainfall determined in conformance with MMAH Supplementary Standard SB-1, "Climatic Seismic Data", Multiplied by the sum of,
 - a) the area in square metres of the horizontal projection of the surface drained, and
 - b) one-half the area in square metres of the largest adjoining vertical surface

15 min Rainfall for Cobourg: 23 mm

Area of horizontal surface draining to sewer: 2200 m² (includes roof of Building D, assumed no controlled roof drains for the purpose of these calculations)

Area of Building D vertical surface: 288 m²

$$Load = 23mm \times \left(2200 + \frac{288}{2} \right)$$

$$Load = 53,912mm \cdot m^2$$

Load = 53,912 litres

As per Table 7.4.10.9, the maximum permitted hydraulic load drained to a horizontal storm drainage pipe is **78,700L** based on a 12-inch sewer at a slope of 1 in 100.

Since the load of 53,912 litres is less than the maximum permitted flow of 78,700 litres, the proposed sewer is acceptable.



Functional Servicing Report
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Appendix C

Sanitary Flow Calculations

Counterpoint Engineering Inc.

Sanitary Design Calculations

Project:	Northumberland Mall	
Project No:	19046	
Location:	Cobourg, ON	
Site ID:	Northumberland Mall	
Site Area:	0.39	ha
Gross Floor Area:	0.09	ha

Average Flow

Commercial	450	L / capita / day
------------	-----	------------------

Equivalent Population (Typical - City of Toronto Design Criteria for Sewers and Watermains, p.34)

Land Use	Population Density (pp/100m ² GFA)	Floor Area (m ²)	Equivalent Residential Population
Commercial	1.1	0.09	10.2

Peaking Factor

Town of Cobourg Design Guidelines, pg. 26

Residential

$$M_d = 1 + \frac{14}{4 + P^{0.5}}$$

3.80	(Maximum)
------	-----------

Extraneous Flows

0.26 l/s/ha

Design Sanitary Flow**

$$Q(d) = \frac{PqM}{86,400} + IA$$

Summary	Peak Flow (l/s)
Average Sanitary Flows	0.0532
Flow From Infiltration	0.1014
Peak Sanitary Flow (With INF)	0.3037



Functional Servicing Report
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Appendix D

Water Demand Calculations

counterpoint engineering

Water Demand Calculations

Project Name: Northumberland Mall
Project Number: 19046

Town of Cobourg Watermain Design Guidelines

Water Demand = Maximum Day Flow + Fire Flow or Peak Hour Flow

Commercial Water Demand

Per Capita Demand	450	L / c / day
Peak Hour Factor	14.13	
Maximum Day Factor	9.5	

Fire Demand

Fire Flow	7,000	L / min	- See FUS calculations.
Fire Flow Duration	1.5	hours	

Commercial Population: 10.2 persons - See Sanitary Flow calculations.
Commercial Demand: 4,590 L / day

Peak Hour Water Demand 64,857 L / day
Total Peak Hour Demand: 64,857 L / day
, or 45 L / min

Maximum Day Water Demand - Residential: 43,605 L / day
Total Maximum Day Water Demand: 43,605 L / day
, or 30 L / min

Total Fire Flow: 7,000 L / min

Maximum Day + Fire Flow: 7,045 L / min
or
1,861 GPM

- Since the Maximum Hour + Fire Flow demand is the highest demand value, this is the one that governs.

counterpoint engineering

Fire Underwriter Survey Fire Flow Calculation

Project Name: Northumberland Mall
 Project Number: 19046

where

$$F = 220C\sqrt{A}$$

F = the required fire flow in litres per minute.
 C = coefficient related to the type of construction.
 = 1.5 for wood frame construction (structure essentially all combustible).
 = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior).
 = 0.8 for non-combustible construction (unprotected metal structural components, masonry or metal walls).
 = 0.6 for fire-resistant construction (fully protected frame, floors, roof).

A = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Legend

Construction Class	Contents Factor
WF wood frame construction	NC non-combustible
OC ordinary construction	LC limited combustible
NC non-combustible construction	C combustible
FC fire-resistant construction	FB free burning
	RB rapid burning

Contents Factor:

Non-Combustible	-25%	Free Burning	+15%
Limited Combustible	-15%	Rapid Burning	+25%
Combustible	No Charge		

Separation	Charge	Separation	Charge
0 to 3m	25%	20.1 to 30 m	10%
3.1 to 10m	20%	30.1 to 45m	5%
10.1 to 20m	15%		

1) Fire Flow

Type of Construction: OC
 C = 1
 A = 929 m²
 F = 6,705 L/min

2) Occupancy Reduction

Contents Factor: C
 Occupancy Reduction = 0%

$$\begin{array}{llll} 0\% & \text{of} & 6,705 \text{ L/min} & = 0 \text{ L/min} \\ \text{F} = 3,646 \text{ L/min} - 912 \text{ L/min} & & = & 6,705 \text{ L/min} \end{array}$$

3) System Type Reduction (to be reduced from result of Step 2)

NFPA 13 Sprinkler: 0% No
 Standard Water Supply: 0% No
 Fully Supervised: 0% No
 Total System Type Reduction = 0%

$$\begin{array}{llll} 0\% & \text{of} & 6,705 \text{ L/min} & = 0 \text{ L/min} \\ & & & \text{(to be reduced from result of Step 2)} \end{array}$$

4) Separation Charge (to be added to result of Step 2)

Building Face	Distance	Charge
North	>45m	0%
East	>45m	0%
South	>45m	0%
West	>45m	0%
Total		0% (max exposure charge can be 75%)

$$\begin{array}{llll} 0\% & \text{of} & 6,705 \text{ L/min} & = 0 \text{ L/min} \\ & & & \text{(to be added to result of Step 2)} \end{array}$$

$$\begin{array}{lll} \text{F} = 7,000 \text{ L/min} & \text{(round to the nearest 1,000 L/min)} & (2,000 \text{ L/min} < \text{F} < 45,000 \text{ L/min}) \\ \text{F} = 1,849 \text{ GPM} & & \end{array}$$